# Oxidation resistance of intermetallic compounds Al<sub>3</sub>Ti and TiAl

Y. UMAKOSHI, M. YAMAGUCHI\*, T. SAKAGAMI, T. YAMANE Department of Materials Science and Engineering, Faculty of Engineering, Osaka University, 2-1, Yamada-Oka, Suita, Osaka 565, Japan

The oxidation kinetics and morphological features of  $Al_3Ti$  and TiAl were investigated. The oxidation resistance of  $Al_3Ti$  is much better than that of TiAl, for example, by a factor of about 30 at 1000° C for 48 h. The big difference in the oxidation resistance is related to the characteristics of the external oxide scales of a protective  $Al_2O_3$  or a mat of crystalline TiO<sub>2</sub> formed on  $Al_3Ti$  or TiAl, respectively. Sufficient aluminium transport from  $Al_3Ti$  assists the formation of the  $Al_2O_3$  scale which acts as a protective film against oxidation. The poor aluminium content of TiAl produces Ti<sub>3</sub>Al phase at the interface of TiAl and oxide scales and increases the diffusion of titanium in the  $Al_2O_3$  scale. The external crystalline TiO<sub>2</sub> scale produced by the diffusion of titanium through the  $Al_2O_3$  scale enhances oxidation of TiAl.

## 1. Introduction

Considerable attention has recently been given to the mechanical and oxidation properties of the aluminides with transition metals which have been used as high-temperature materials of superior strength-to-weight ratio in aircraft and/or automobile parts [1]. One of the candidates for low density-high strength intermetallic compounds used at high temperatures exists in the Al-Ti system. In this system there are three intermetallic compounds or ordered alloys such as  $Ti_3Al$ , TiAl and  $Al_3Ti$ . The deformation behaviour of these compounds have been extensively investigated and the difficulty for industrial application is overcome by improvement of their ductility [2–11].

Recently,  $Al_3$ Ti has been expected to be a potential candidate for a low-density high-temperature structural material itself, and also a good coating material, because its greater aluminium content gives a lower density and probably better oxidation resistance than TiAl [10, 12]. TiAl and Ti<sub>3</sub>Al have been reported to exhibit on poor resistance to oxidation at high temperatures above about 800° C, because the external layer of those compounds is not a protective Al<sub>2</sub>O<sub>3</sub> film, but TiO<sub>2</sub> or a mixture of TiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> [12]. When the surface is coated with Al<sub>3</sub>Ti, a protective Al<sub>2</sub>O<sub>3</sub> film can be expected to form and increase the oxidation resistance.

In this paper we present the isothermal oxidation kinetics and resistance of the intermetallic compounds Al<sub>3</sub>Ti and TiAl. The morphology of the oxides and the alloy formed on the compounds are also reported.

## 2. Experimental details

Pure titanium (99.9%) and aluminium (99.99%) were melted in a high-purity argon plasma furnace to prepare intermetallic compounds TiAl containing 35 wt % Al and Al<sub>3</sub>Ti containing 37.3 wt % Ti. Al<sub>3</sub>Ti single-phase specimens were carefully prepared by remelting and solidification of the master ingot in Ar-10% H<sub>2</sub> gas atmosphere because of its narrow composition. Thin sheets  $(10 \text{ mm} \times 10 \text{ mm} \times 1 \text{ mm})$ were cut from the cast ingot and their surfaces were electrically polished after grinding with metallographic polishing papers. Isothermal oxidation tests were carried out at temperatures between 800 and 1000°C in pure oxygen gas flowing at a rate of  $200 \,\mathrm{ml}\,\mathrm{min}^{-1}$  at atmospheric pressure. Weight gains due to oxidation were examined by thermogravimetric analysis. The microstructure of the oxide scales and/or the alloy formed at the interface was observed by scanning electron microscopy and the microanalyses of the principle elements (Al, Ti) were also done by energydispersive X-ray (EDX) analyses. Crystal structure was confirmed by X-ray diffractometry measurement.

#### 3. Results and discussion

Fig. 1 shows the variation of weight gain per unit area of TiAl compounds with the oxidation time at various temperatures. In the early stages of oxidation, the curves show a parabolic shape indicating formation of a protective oxide thin scale against oxidation, probably  $Al_2O_3$  scale. After the initial transient period, the curves become linear and the slope of the curves increases with increasing temperature. In particular, weight gain increases at great speed at 1000° C. The transient period from the parabolic to the linear part is shortened with increasing temperature.

For comparison with the oxidation kinetics of  $Al_3Ti$ and TiAl, the weight gain-oxidation time curves of both compounds at 900 and 1000° C are shown in Figs 2 and 3. It is obvious that the oxidation resistance of  $Al_3Ti$  is much better than that of TiAl. The tendency

\*Present address: Department of Metal Science and Technology, Kyoto University, Sakyo-ku, Kyoto 606, Japan.



Figure 1 Thermogravimetric results for weight gain per unit area of TiAl as a function of annealing time, when exposed to oxygen at various temperatures.

becomes more remarkable at higher temperatures. The oxidation of Al<sub>3</sub>Ti is much slower than that of TiAl, for example, roughly by a factor of 30 at 1000° C for 48 h. The weight gain-time relationship of Al<sub>3</sub>Ti was proved to be still controlled by a parabolic rate law in the form of parabolic plots even at 1000° C. Thus, the big difference in the kinetics of oxidation of Al<sub>3</sub>Ti and TiAl can be attributed to the morphology and the characteristics of the oxide scales.

Fig. 4 shows a scanning electron micrograph and the EDX analyses of a cross-section of oxide scales formed on the TiAl exposed to oxygen at  $1000^{\circ}$  C for 48 h. The external layer of the oxide scales is TiO<sub>2</sub> and the mixture of  $Al_2O_3$  and  $TiO_2$  can be observed under the  $TiO_2$  layer. Large numbers of voids and pores are formed in the phase of the mixture of  $Al_2O_3$  and  $TiO_2$ . In the early stages of oxidation of TiAl,  $Al_2O_3$  film must be formed on the surface but it does not effectively as a protective oxide scale against further oxidation because of the high diffusivity of titanium in the  $Al_2O_3$ scale, and the nucleation and growth of  $TiO_2$  phase in the  $Al_2O_3$  scale produces many pores. Numerous pores and oxide scales which were embedded as a diffusion marker are observed at the initial surface of TiAl, indicated by a white arrow in Fig. 4. Under the initial surface of TiAl, oxide scales are also observed



*Figure 2* Variation of weight gain per unit area with oxidation time of  $Al_3Ti$  and TiAl oxidized in oxygen at 900° C.



Figure 3 Variation of weight gain per unit area with oxidation time of  $Al_3Ti$  and TiAl oxidized in oxygen at 1000° C.

which shows oxygen can also diffuse to the TiAl compound. The poor aluminium content in TiAl during oxidation produces  $Ti_3Al$  at the oxide/metal interface. Even after short periods of oxidation,  $Ti_3Al$  can be observed. The existence of  $Ti_3Al$  may accelerate the penetration of titanium in the  $Al_2O_3$  phase and therefore the oxidation resistance of TiAl will fall. The general microstructural and morphological features of the oxide scales and the  $Ti_3Al$  phase at the interface, are almost the same at the test temperatures, although there is a difference in the growth rate of the oxide scales and the  $Ti_3Al$  phase.

The crystal structure of the oxide scales and the intermetallic compounds for the TiAl specimen annealed in oxygen at 1000° C for 48 h was examined

(Fig. 5).  $Al_2O_3$  and  $TiO_2$  scales have  $D5_1(\alpha - Al_2O_3)$  and C4-type structure, respectively, and  $Ti_3Al$  phase has  $D0_{19}$ -type ordered structure. Although the surface of the oxidized TiAl sheet was X-ray irradiated, all the oxidation products could be examined because the substrate TiAl was confirmed to have an  $L1_0$  type ordered structure from the diffraction patterns. The average composition of the mixture of  $Al_2O_3$  and  $TiO_2$  scales observed in Fig. 4 corresponded to that of the complex oxide  $Al_2TiO_5$  but the X-ray diffraction patterns did not show any evidence of the presence of  $Al_2TiO_5$ .

The morphology of the surface oxide films because its affect on adherence and spallation is very important in maintaining the nature of the oxide film as a



Figure 4 Scanning electron micrograph and energy-dispersive X-ray analyses of a cross-section of TiAl oxidized in oxygen at 1000°C for 48 h.



Figure 5 X-ray diffraction spectra of the TiAl specimen oxidized in oxygen at 1000°C for 48 h.

protective diffusion barrier. The surface microstructure of oxide films produced on TiAl and Al<sub>3</sub>Ti compounds is given in Fig. 6. The oxide scale formed on Al<sub>3</sub>Ti has a fine microstructure and a smooth surface. Even during the cooling and heating process, the good adherence of the oxide film to Al<sub>3</sub>Ti was maintained. On the other hand, the external surface of TiAl was covered with a mat of fine crystals of TiO<sub>2</sub>. The crystal growth of randomly oriented rod-like grains of TiO<sub>2</sub> leads to the formation of numerous voids and pores at the grain boundaries which trigger crack initiation and spallation of oxide films from the alloy substrate. The spallation of the crystalline TiO<sub>2</sub> layer is enhanced by the thermal cycling, resulting in the acceleration of oxidation.

 $Al_3Ti$  has been shown in Figs 2 and 3 to exhibit much better oxidation resistance than TiAl. Fig. 7

shows a scanning electron micrograph of a crosssection of Al<sub>3</sub>Ti exposed to oxygen at 1000° C for 48 h. The results of EDX analyses are also given in the figure. The external oxide scale consists of almost all  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> and no intermetallic compound can be observed at the interface between Al<sub>3</sub>Ti and oxide scale, although a crevice induced during preparation of the EPMA specimen is seen. Because of its greater aluminium content, sufficient aluminium transport from Al<sub>3</sub>Ti takes place for the growth of a protective  $Al_2O_3$  layer to occur even during a long period of annealing at high temperatures. Low titanium content in the Al<sub>2</sub>O<sub>3</sub> layer hinders the nucleation of TiO<sub>2</sub> phase and the formation of voids and pores. The absence of the high titanium content Ti<sub>1</sub>Al compound at the interface with Al<sub>3</sub>Ti causes a big difference in the oxidation resistance between Al<sub>3</sub>Ti and TiAl.



Figure 6 Scanning electron micrographs of the surface oxide scales formed on Al<sub>3</sub>Ti and TiAl. (a)  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> scale formed on Al<sub>3</sub>Ti exposed to oxygen at 1000° C for 48 h. (b) TiO<sub>2</sub> scale formed on TiAl exposed to oxygen at 1000° C for 48 h.



*Figure 7* Scanning electron micrograph and energy-dispersive X-ray analyses of Al<sub>3</sub>Ti oxidized in oxygen at 1000° C for 48 h.

Therefore,  $Al_3Ti$  can be used as a good coating material for the compound TiAl and some dilute alloys with a TiAl-base, similar to other aluminides used as coating materials such as NiAl and FeAl. The  $Al_3Ti$  coating would be effective for protecting the titanium- and TiAl-based alloys against oxidation at high temperatures. Aluminizing of titanium and titanium-aluminium alloys can be accomplished by conventional methods which include slurry spraying, molten dipping and pack cementation. A well-adhering coating layer of  $Al_3Ti$  can be obtained without difficulty because of the much faster diffusivity in  $Al_3Ti$  than in other aluminides of titanium.

#### 4. Conclusions

1. The weight gain-time curves of  $Al_3Ti$  oxidation show a parabolic relation even at 1000° C.

2. In the early stages of oxidation,  $Al_2O_3$  scale may be formed on TiAl but it cannot act as a protective film in further stages because of the high diffusivity of titanium in the  $Al_2O_3$  scale, resulting in the formation of TiO<sub>2</sub> crystalline phase as an external scale.

3. Ti<sub>3</sub>Al was formed at the interface of TiAl and oxide scale during oxidation, because of the poor aluminium content of TiAl. The penetration of titanium and the formation of TiO<sub>2</sub> in the Al<sub>2</sub>O<sub>3</sub> scale may be accelerated by the existence of Ti<sub>3</sub>Al. Numerous pores in the mixture of Al<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> scales also hinder the oxidation resistance.

4. The oxidation resistance of  $Al_3Ti$  is much better than that of TiAl, and the tendency becomes more remarkable with increasing test temperatures.

5. Al<sub>3</sub>Ti can be used as a good coating material

against oxidation for the titanium- and TiAl-based alloys.

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### References

- H. A. LIPSITT, in "High Temperature Ordered Intermetallic Alloys", edited by C. C. Koch, C. T. Liu and N. S. Stoloff (MRS, Pittsburgh, 1985) p. 351. This work was partly supported by Research Foundation for Materials Science.
- 2. D. SHECHTMAN, M. J. BLACKBURN and H. A. LIP-SITT, Met. Trans. 5 (1974) 1373.
- 3. S. M. L. SASTRY and H. A. LIPSITT, *ibid.* 8A (1977) 1543.
- 4. W. J. S. YANG, *ibid.* **13A** (1982) 324.
- 5. Idem, J. Mater. Sci. Lett. 1 (1982) 199.
- 6. R. E. SCHAFRIK, Met. Trans. 7B (1976) 713.
- 7. R. J. KERANS, ibid. 15A (1984) 1721.
- 8. T. KAWABATA, T. KANAI and O. IZUMI, Acta Metall. 33 (1985) 1355.
- 9. M. YAMAGUCHI, Y. UMAKOSHI and T. YAMANE, *Phil. Mag.* **55A** (1987) 301.
- 10. M. YAMAGUCHI and Y. UMAKOSHI, *Mater. Res.* Soc. Symp. Proc. **81** (1987) 275.
- 11. Y. UMAKOSHI, M. YAMAGUCHI and T. YAMANE, *Phil. Mag.* **58A** (1988) 651.
- 12. M. KABBAJ, A. GALERIE and M. CAILLET, J. Less-Common Metals 108 (1985) 1.

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